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(71) Applicant (for all designated States except US): SCOT IN-CORPORATED [US/US]; 2525 Curtiss Street,, Downers Grove, IL 60515 (US).

(71) Applicant and

(72) Inventor: JORDAN, Clifford, L. [US/US]; 525 North Rose Street, Park Ridge, IL 60068 (US).

(74) Agent: BUSHNELL, Robert, E.; Robert E. Bushnell & Law Firm, Suite 300, 1522 K Street, N.W., Washington, DC 20005-1202 (US).

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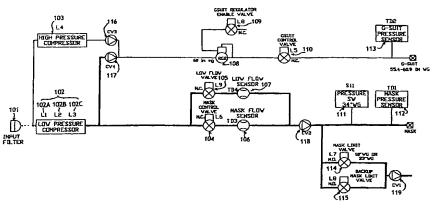
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(54) Title: COMBINED AIRCREW SYSTEMS TESTER (CAST)



(57) Abstract: The present invention enables functional testing nearly all aircrew equipment including a COMBAT EDGE (combined advanced technology enhanced design "G" ensemble) system of components which include a mask, a G-suit, communication systems, and a goggle. The present invention includes a gas system which includes an input filter (101), a first compressor (102) comprising at least one blower, preferably three blowers connected in series, a second compressor (103), a first flow sensor (106), a second flow sensor (107), a first flow valve (104), a second flow valve (105), a regulator (108), a first pressure sensor (112), a second pressure sensor (113), a first pressure valve (110), a second pressure valve (114), and a controller. The inlet filter (101) is designed to accept a chemical filter. The second compressor (103) produces a lower flow at a higher pressure than the first compressor (102). This combination works particularly well when inflating the G-suit because when the G-suit inflates, initially there is a large change in volume without much change in pressure, and then, as the G-suit fills out and becomes firm, the change in volume slows down and the rate of the pressure increases. The present invention includes a digital indicator. A method of operating the tester and the gas system are also disclosed. The present invention includes a normal breathing test, a preflight test, a G-suit leak test and two dynamic flow leak tests. The communication system test and goggle test are further included.

TITLE

COMBINED AIRCREW SYSTEMS TESTER (CAST)

CLAIM OF PRIORITY

[0001] This application makes reference to, incorporates the same herein, and claims all benefits accruing under 35 U.S.C. §119 from a provisional application entitled *Combined Aircrew Systems Tester (CAST)* filed in the United States Patent & Trademark Office on 1 August 2001, and there duly assigned Serial No. 60/308,846 and my U.S. patent application entitled *COMBINED AIRCREW SYSTEMS TESTER (CAST)* filed in the United States Patent & Trademark Office on 31 July 2002, and there duly assigned Serial No. 10/208,188 by that Office.

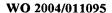
BACKGROUND OF THE INVENTION

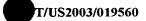
Field of the Invention

[0002] The present invention relates to a combined aircrew systems tester, and more particularly, to a combined aircrew systems tester enabling functional testing of aircrew equipment.

Description of the Background Art

[0003] Life support systems are very crucial for members of an aircrew of aircraft and especially high performance aircraft. Life support systems include COMBAT EDGE (combined advanced technology enhanced design G-ensemble) system components. The system includes a G-suit, an oxygen mask, goggles, and a communication equipment. Specifically, the COMBAT EDGE system includes the MBU-20/P Oxygen Mask, CSU-17/P





Vest Assembly, HGU-55/P Helmet with occipital bladder, CRU-94/P Integrated Terminal Block or PBG (pressure breathing for Gs) Chest Mounted Regulator or both CRU-94/P Integrated Terminal Block and PBG Chest Mounted Regulator, and all associated Anti-G garments.

[0004] Life support systems are very important for the aircrew and therefore, it is extremely important that such vital systems be properly tested. If any of the above systems do not work, a pilot for instance may be unable to control the aircraft.

[0005] Earlier systems had different testing units for each type of life support. A separate cumbersome unit would be needed for testing an oxygen mask and another separate large unit would be needed for testing the anti-G suit. This is expensive and very awkward for users to test their equipment at different stations while for instance they are wearing such equipment. Moreover, the power sources for such equipment are usually not commonly available because of the high power necessary to drive such complicated devices.

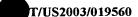
[0006] Particularly, a conventional tester for an oxygen mask requires a separate high pressure source of breathing air/oxygen. It is awkward for users to bring the tester and the separate high pressure source.

[0007] For the foregoing reasons, there is a need for a tester that can be inexpensively and efficiently test life support equipment.

SUMMARY OF THE INVENTION

[0008] It is therefore an object of the present invention to have an integrated unit that can functionally test the various aircrew equipment.

[0009] It is another object to have an aircrew systems tester that can test all of the aircrew life support equipment and communication systems.



[0010] It is yet another object to have a unit that can test the aircrew life support equipment and yet not require much power for operation.

[0011] It is still yet another object to have a unit that tests the aircrew life support equipment and yet not require high pressure air/oxygen cylinders.

[0012] It is still another object to have a unit that tests the aircrew life support equipment and significantly reduces supporting man-hours, deployment costs and mobility footprint.

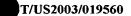
[0013] It is still further another object to have a life support system tester that is able to operate in a chemical warfare environment.

[0014] To achieve the objectives of the present invention, there is provided a tester including a gas system which includes an input filter located in an inlet port, the input filter filtering an air to prevent foreign particles from entering the gas system, a first compressor compressing the air, the first compressor comprising at least one blower, a speed of the blower depending on a voltage applied to the blower, a second compressor compressing the air, the second compressor producing a lower flow than the first compressor, the second compressor producing a higher pressure than the first compressor, a first flow sensor detecting a flow of the compressed air and a leaking of the aircrew systems, a second flow sensor detecting the flow of the compressed air and the leaking of the aircrew systems, a first flow valve mounted for controlling the flow of the compressed air to the first flow sensor, a second flow valve mounted for controlling the flow of the compressed air to the second flow sensor, a regulator regulating a pressure of the second system, a first pressure sensor detecting a pressure of the mask, a second pressure sensor detecting the pressure of the second system, a first pressure valve for controlling the pressure of the first system, a second pressure valve for controlling the pressure of the second system, and a controller controlling an operation of the gas system.



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The inlet filter designed to accept a C2 (chemical) filter. The gas system is particularly suitable for testing a mask and a G-suit. It is preferred that the first compressor comprises three regenerative blowers, a first blower, a second blower, and a third blower, connected in series. It is preferred that each of the three regenerative blowers has 21 inch H₂O of a maximum output pressure. In a preferred embodiment, the first compressor compresses the air until a G-suit pressure reaches 55 inch H₂O, the second compressor starts to compress the air when the G-suit pressure is about 55 inch H₂O and finishes when the G-suit pressure is about 70 inch H₂O. The first flow sensor is able to measure the flow from 0 to 10,000 cc/min (cubic centimeters per minute), and the second flow sensor is able to measure the flow 0 to 300 cc/min. The first flow valve and the second flow valve determine which sensor is used. The gas system further includes a digital indicator reading out data outputted from the first and second flow sensors. The gas system further includes a first limit valve for limiting a pressure of the first system. The operation of the gas system is controlled by a main printed circuit board (PCB) which uses CMOS (complementary metal oxide semiconductor) logic. The present invention further includes a speed control printed circuit board (PCB) which controls the first compressor by controlling a voltage applied to the second compressor. The tester of the present invention includes a first unit for testing a mask, a second [0015] unit for testing a G-suit, and a third unit for testing a communication system. The tester can further includes a fourth unit for testing a goggle. Since the tester of the present invention is self contained and integrated, a control panel of the tester of the present invention has a plurality of switches and indicators for controlling the tests for the life support systems of an aircrew member. The third unit preferably includes an input accommodating a microphone, an input accommodating headset, and two inputs for carbon microphones. The third unit further includes a built-in continuity tester. The third unit can further includes an



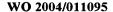
accommodation of a second headset and microphone accommodating a first user to communicate with a second user.

[0016] A method of operating a gas system for testing aircrew systems which includes a mask and a G-suit is comprised of the steps of selecting a test mode between the test mode for the normal breathing and the test mode for the PBG breathing, filtering an ambient air with a C2 filter, compressing the air, detecting a flow of the air, and detecting a pressure of the mask or G-suit. When the mask test mode is selected, the step of compressing the air further includes the step of turning on the first compressor. When the PBG mode test is selected, the step of compressing the air further includes the steps of turning on the first compressor until a G-suit pressure reaches 55 inch H₂O, turning off the first compressor and turning on the second compressor when the G-suit pressure is about 55 inch H₂O, and turning off the second compressor when the G-suit pressure is about 70 inch H₂O. The first compressor is controlled by adjusting a voltage applied to each of the first, second, and third blowers and by deciding how many blowers are turned on.

[0017] With this configuration, the present invention enables functional testing of nearly all aircrew equipment including the COMBAT EDGE (Combined Advanced Technology Enhanced Design "G" Ensemble) system components.

BRIEF DESCRIPTION OF THE DRAWINGS

[0018] A more complete appreciation of this invention, and many of the attendant advantages thereof, will be readily apparent as the same becomes better understood by reference to the following detailed description when considered in conjunction with the accompanying drawings in which like reference symbols indicate the same or similar components, wherein:





[0019] Fig. 1 illustrates a functional diagram of a gas system of the present invention;

[0020] Fig. 2 illustrates the control panel of the present invention;

[0021] Fig. 3 illustrates an overall block diagram of the present invention;

[0022] Fig. 4A through 4S illustrate schematic diagrams of sections 4A through 4S, respectively of Fig. 3 of the present invention; and

[0023] Fig. 5 illustrates a general block diagram of a portion of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0024] The present invention is an integrated unit that can functionally test the various aircrew equipment. Life support systems include COMBAT EDGE (combined advanced technology enhanced design G-ensemble) system components. The system includes the MBU-20/P Oxygen Mask, CSU-17/P Vest Assembly, HGU-55/P Helmet with occipital bladder, CRU-94/P Integrated Terminal Block or PBG (pressure breathing for Gs) Chest Mounted Regulator or both CRU-94/P Integrated Terminal Block and PBG Chest Mounted Regulator, and all associated Anti-G garments.

[0025] A functional diagram of a gas system for a combined aircrew system tester (CAST) is shown in FIG.1.

[0026] The gas system of the tester provides two air sources. One is for a mask or a vest, and the other is for a G-suit (a suit designed to counteract the physiological effects of acceleration on an aviator or astronaut - called also called an anti-G suit). The air for the G-suit is provided through a G-suit port and the air for the mask/vest through the mask port. These air sources are used to perform maintenance and preflight testing of the pilot's life support equipment. The mask port air is used to test the pilot's oxygen mask and COMBAT EDGE gear. There are two modes of mask testing, 'normal' and 'PBG' (Pressure Breathing

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for G (acceleration force of gravity)).

[0027] Referring to Figs. 1 through 4, air for the mask starts by passing through an input filter 101. The ambient air is inputted through an inlet port. A screen mesh filter assembly screws into the inlet port to prevent particles from entering the air stream. The thread on the inlet port is designed so that it can accept a C2 (chemical) filter 246 used for chemical warfare. This feature makes it possible to use the tester in a chemical environment. All the air outputted by the tester passes through the C2 when it is installed.

[0028] Then, the air for the mask is compressed by a low-pressure compressor system 102. [0029] The low-pressure compressor system 102 includes at least one blower but preferably includes at least three regenerative blowers 102a, 102b and 102c connected in series to generate the necessary pressure and flow. The output pressure is determined by the speed of the blowers 102a, 102b and 102c and how many blowers 102a, 102b and 102c are turned on. The voltage applied to each of the blowers 102a, 102b and 102c controls the speed. If the voltage decreases, the speed decreases and the output pressure is decreased. The voltage is controlled by a speed control circuit, which is part of the speed control PCB (Printed Circuit Board, PCB3).

[0030] Then, the air for the mask passes through one of two flow sensors 106, 107, which are used to alert the user that his or her equipment is leaking and to measure the leak rate. One flow sensor is a high flow sensor 106 which measures flow from 0 to 10,000 cc/min (cubic centimeters per minute) and the other flow sensor is a low flow sensor 107 which measures flow from 0 to 300 cc/min. A mask control valve 104 and a low flow valve 105 determine which sensor is used. One of two valves 104 and 105 which are normally closed is open to permit the air to flow through one of the flow sensors 106 and 107. The output from the flow sensor 106 or 107 is fed into a digital indicator 274 (FIG.2) to indicate flow. The indicator 274



reads out in the appropriate units. Its range is set by an embedded processor on a main PCB (Printed Circuit Board, PCB1).

[0031] These sensors are excited with 10.0 VDC (voltage of direct current). At zero flow their output is 1.0 VDC (voltage of direct current). At full scale the output is 5.0 VDC (voltage of direct current). The low flow sensor 107 is not quite linear. To compensate for this, five linear curves are fitted to the flow versus voltage curve. The slopes of these five curves are programmed into the digital indicator 274 that is used to indicate flow.

[0032] Next, the air passes through a check valve 118 and flows out the mask port 242. The check valve 118 prevents foreign materials from entering the gas system of the tester. A pressure switch 111 and a mask pressure sensor 112 monitor the mask port pressure. They are used to control and limit the mask port pressure. The mask pressure sensor 112 converts pressure to voltage. The voltage is fed into the digital indicator 270 where it is converted to a digital signal, which is presented as number scaled in engineering units. This number is updated 13 times a second. The indicator has three logic high outputs, which output when the pressure exceeds their set pressure. In addition, the pressure switch 111 is connected to the mask pressure sensor 112. The pressure switch 111 is normally closed, and is preferably set to open at 18 in (inch) H₂O.

[0033] A mask limit valve 114 and a backup mask limit valve 115 are also provided for controlling the mask port pressure.

[0034] The air for the G-suit is produced by multiple compressors 102a, 102b, 102c and 103. At pressures below 55 in H₂O, the low-pressure compressor system 102 compress the air. At pressures above 55 in H₂O, a high-pressure compressor 103 compresses the air. This is done to minimize the amount of time to inflate the G-suit. The low-pressure compressors



(with regenerative blowers) 102a, 102b and 102c produce high flow at relatively low pressures while the high-pressure compressor 103 produces low flow but can compress the air to a higher pressure. This combination works particularly well when inflating the G-suit because when the G-suit inflates, initially there is a large change in volume without much change in pressure, and then, as the G-suit fills out and becomes firm, the change in volume slows down and the rate the pressure increases.

[0035] A G-suit regulator enable valve 109 and a G-suit regulator 108 are provided for regulating the G-suit pressure. The G-suit regulator enable valve 109 is normally closed. When the G-suit pressure increases up to a certain pressure, the G-suit regulator enable valve 109 is opened to vent the G-suit regulator 108.

[0036] A G-suit control valve 110 is further provided for controlling the G-suit pressure.

[0037] With this configuration, the present invention does not require a separate high pressure source of breathing air and oxygen.

[0038] As explained above, the present invention is self contained. Thus, a control panel of the combined aircrew systems tester of the present invention has a plurality of switches and indicators for controlling the tests for the life support systems of an aircrew member.

[0039] FIG. 2 shows a preferred embodiment of the control panel.

[0040] As shown in Fig. 2, the control panel 200 includes a 'mode select' switch 201, a 'pressure select' switch202, a 'test select' switch 203, and a 'press to test' switch 204.

[0041] The mode select portion 201 includes a mode select switch 201A preferably provides for two dynamic flow leak testing (high leak ('LK-HI') 201D and low leak ('LK-LO') 201C), a G-suit leak testing ('LK-GS') 201B, and one mask testing ('mask') 201E.

[0042] The pressure select switch 202 is preferably provided for 41M, 43M, or 45M (where



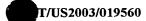
M stands for 1000). Thus, the air is provided at one of four positive pressures; normal, 41M, 43M, or 45M.

[0043] The test select switch 203 provides for a PBG breathing testing ('PBG'), a normal breathing testing ('normal'), and 'off'. The test select switch 203 is preferably a three-position toggle switch. The test select switch 203 drives two de-bouncers 332, 334, the PBG and the normal logic steps.

[0044] A leaking indicator 235 is also included in the control panel 200.

[0045] The communication section includes audio input A 222 and B 224, a carbon headset input 226, a press to test ('PTT') jack 228, a continuity status of a microphone 230, a continuity status of the earphone 232, a microphone "on" indicator 234, an audio select switch 236 that can be switched to continuity test mode 236a, 'LIS/TLK 1' (listen/talk 1) 236b, or 'LIS/TLK 2' 236c. A port for the goggle 238 and a 'G-suit' button 240 are included along with a mask port 242. Indicators 244a and 244b relating to the PBG (pressure breathing for Gs) are also included. Reference 244b indicates that 'PBG timed out', 244a indicator concerns the 'PBG'. The control panel 200 also includes the filter 246. There are ports for the power 248 and the battery 250. A switch or indicator for tare 252 is along with a hold 254, and a reset 256 indicator or switch. A G-suit ready indicator 258 is also included along with a G-suit testing on/off switch 260 and a pressure control knob 262. The tester also includes a G-suit port pressure displays 268, a mask port pressure display 270, a time display 272, and a high and low flow display 274. The displays can be a digital display such as light emitting diodes, or liquid crystal display or other types of indicators.

[0046] The operation of the tester is explained in more details as follows.



[0047] To test the mask when the aircrew does not wear COMBAT EDGE, the user selects a mask mode of operation by pressing the mode select switch 201. The user selects a desired breathing pressure by pressing the pressure select switch 202. Then the test select switch 203 is toggled to the 'normal' position, which starts air flow out of the mask port at slight positive pressure. Then the press to test button 204 is pushed to cause the air pressure to increase to the pressure selected. The air is preferably provided at one of four positive pressures; normal, 41M, 43M, or 45M. When the mask mode has been selected and the test select switch is in the 'normal' position, the mask control valve 104 opens permitting the air to flow out the mask port. When operating in the normal mask mode, the air outputted through the mask port is provided at a pressure from 1 to 10 in H₂O.

[0048] The PBG (Pressure breathing for G) breathing is used to perform preflight tests and fit tests while the users are wearing COMBAT EDGE. The users wearing COMBAT EDGE are required to take the preflight test on their masks at PBG breathing pressure level. This test is performed at a breathing pressure of 16 in H₂O with the G-suit not inflated. When the G-suit is not inflated, it is dangerous to breathe air at pressures much above 16 in H₂O. When the mode select switch 201 is set to 'mask' and the test select switch 203 is in the 'PBG' position, the air flows from mask port at normal pressure. When the press to test button 204 is depressed, the breathing pressure increases to 16 in H₂O. The user verifies that he or she is breathing normally, verifies proper mask functions and notes that their vest starts to inflate. Then the user momentarily stops breathing to test a leak. A light of the leaking indicator 235 will go out if there are no leaks greater than 5.5 lpm (liters per minute). When the press to test button 204 is pressed, the speed of the low-pressure compressor system 102 increases.

[0049] After a user is initially fitted with COMBAT EDGE equipment, a fit test is performed. This test is similar to the preflight test except the fit test is performed at 32 in H₂O. The user has to be sitting down to perform this test. The fit test starts by performing the preflight test. Then the mask port pressure is increased slowly to 32 in H₂O by adjusting the pressure control release and knob 262 until the air pressure reaches 32 in H₂O. Then the preflight test is repeated.

[0050] During preflight and fitting a red light turns on when flow exceeds 5.5 lpm. The user momentarily holds his or her breath to check for leaks. If there are no leaks, the leak light is turned off.

[0051] The voltage from the low flow sensor 107 is compared with a preset voltage that is equivalent to the sensor output when the flow is 5.5 lpm. When the voltage exceeds the preset voltage, the light of the leaking indicator 235 is turned on.

[0052] In order to do the preflight test safely, the G-suit has to be inflated. The low-pressure compressor system 102 and the high-pressure compressor 103 provide the air for the G-suit. When the G-suit switch 260 is turned on, the G-suit control valve 110 opens and the low-pressure compressor system 102 is turned on at its maximum operating speed so that the air rapidly fills the G-suit to its final approximate shape. When the G-suit pressure reaches 55 in H₂O, as sensed by G-suit pressure sensor 113, the high-pressure compressor 103 takes over filling the G-suit to its final pressure. The output of the G-suit pressure sensor 113 is fed into the digital indicator/controller 268. The indicator 268 turns the input voltage into a digital signal and processes it, rescaling it into engineering units and outputting it in the form of a number presented on the indicator. The G-suit pressure is maintained at 60 in H₂O by the G-suit regulator 108. If the G-suit pressure exceeds 70 in H₂O, the high-pressure compressor 103

is turned off to limit the G-suit pressure to 70 in H_2O . After the G-suit pressure stabilizes at 60 in H_2O , the user turns off the G-suit switch 260.

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[0053] The G-suit is periodically checked for leakage. To do this, the G-suit is pressurized to 138.4 in H₂O (5 psi, pounds per square inch) and monitored for a change in pressure over an interval of time.

[0054] When the mode select switch 201 is in 'LK-GS' and the G-suit switch 260 is turned on, the G-suit regulator enable valve 109 is turned on to disable the G-suit regulator 108, allowing the G-suit pressure to rise to pressures greater than 60 in H_2O , which is a normal G-suit operating pressure. The high-pressure compressor is turned off at 138.4 in H_2O . When the pressure reaches 138.4 in H_2O , the power to the G-suit control valve 110 and the high-pressure compressor 103 is turned off to limit the pressure to 138.4 in H_2O . Once the pressure stabilizes, the user turns off the G-suit switch 260 to close off the G-suit. The tare switch 252 is pushed for zeroing the time and G-suit pressure. At 120 seconds the hold button 254 is pressed for holding the indicated change in time and change in G-suit pressure. From these changes, the leak rate can be obtained.

[0055] When the mode select switch 201 is in the 'LK-HI' position (indicator 201D), the mask control valve 104 is opened. The low flow valve 105 remains off for directing all the flow through the high flow sensor 106.

[0056] When the mode select switch 201 is in the 'LK-LO' position (indicator 201C), the mask control valve 104 is closed. The low flow valve 105 is turned on for directing all the flow through the low flow sensor 107.

[0057] A second method used to verify the oxygen equipment seals is to measure a drop in



pressure over an interval of time. The component under the test is attached to the mask port and is pressurized to 32 in H₂O by setting the mode to 'mask' and the test select switch 203 to 'PBG'. The press to test button 204 is pushed and the pressure control knob 262 is adjusted until air pressure reaches 32 in H₂O. After the pressure has stabilized, the press to test button 204 is released to cut off the air source. The tare switch 252 is pressed to start a timer and zero the pressure indicator, 268 and 270. At a prescribed time the hold switch 254 is pressed to hold the timer and the pressure indicator readings. If the change in pressure is less than a prescribed amount in the prescribed time, the leak rate is within tolerance.

[0058] The present invention is designed to address safety issues with the following features.

[0059] When performing COMBAT EDGE testing, it is necessary to expose the user to excessive breathing pressures. Exposure to excessive breathing pressure can hurt the user. It is only safe under curtain conditions and for limited periods of exposure. Under no circumstance should the breathing air pressure exceed 34 in H₂O.

[0060] The present invention compresses the filtered ambient air to pressures close to the maximum allowable output mask pressure, while the conventional testers start with air that is compressed to pressures that are orders of magnitude greater than the maximum allowable output mask pressure. If the step down regulation system in the conventional pressures completely fails, the user is exposed to pressures that many times greater than what is safe. On the other hand, the user of the present invention would be exposed to pressures not higher than the maximum allowable mask output pressure.

[0061] As stated before, the blowers 102a, 102b, and 102c provide the breathing air. The maximum pressure that can be developed by each of the blowers 102a, 102b, and 102c is 21



in H_2O when being driven by main power supply voltage at zero flow. If all pressure limiting systems were to fail, the maximum breathing pressure that could be developed to 63 in H_2O at zero flow, which is comparable to the maximum safe pressure of 34 in H_2O . When the user is breathing, the pressure is significantly less.

[0062] Another safety feature of the present invention is a mask pressure limiting system. In the preflight test, if the pressure increases above 18 in H₂O, the power to the mask limit valve 114 is cut, venting the system through a check valve 119. This check valve 119 prevents back flow through the mask limit valve 114 when the user is inhaling. In addition, the mask port pressure is limited to 34 in H₂O under all circumstances. The backup mask limit valve 115 operating current is passed through a pressure limit switch 111 set to open at 34 in H₂O. The backup mask limit valve 115 is a normally open valve. When the pressure limit switch 111 opens, the operating current is interrupted to open the backup mask limit valve 115.

[0063] The method of controlling the CAST is described in more detail below. Fig. 4A through 4S illustrate schematic diagrams of sections 4A through 4S, respectively of the overall block diagram of Fig. 3 of the present invention. The schematics of 4A through 4S are sectioned to show the entire schematic of the present invention. Some portions may overlap in order to accurately show the connections between the individual elements.

[0064] The operation of the gas system is controlled by the main printed circuit board (PCB 1), which uses CMOS (complementary metal oxide semiconductor) logic to control the overall operation. There are two pressure sensors, two digital indicators, five switches and one potentiometer that input and drive the logic functions located on the main PCB (Printed Circuit Board, PCB1). The logic outputs control the speed control PCB (PCB3), and the

valves that control flow.

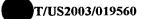
[0065] All logic inputs are derived from either switch closures or TTL (transistor-transistor logic) located in the digital indicators. They pass through de-bouncers. The de-bouncers clean up these inputs and turning them into single pulse square waves with CMOS logic high levels.

[0066] The outputs refer to either compressor motors or valves. The valve outputs and the high-pressure compressor output are located on the main PCB (PCB1). They include an opto isolator and power relays. This is done to protect the CMOS logic from inductive spikes that occur when switching a valve. The high-pressure compressor output is located on the main PCB (PCB1) and the low-pressure compressors outputs are located on the speed control PCB (PCB3).

[0067] A mode select circuit includes the mode select switch 201, a momentary push button driving a Johnson Counter (also known as a twisted-ring counter) (see FIG. 4D). The Johnson counter provides the 'MASK' for the mask testing, 'LK-HI' for the high-leak testing, 'LK-LO' for the low leak testing, and 'LK-GS' for G-suit leak testing. It drives four buffers, which drive four LEDs (light emitting diodes) 201B, 201C, 201D, 201E, which indicate the mode that is selected. The pressure select circuit works the same way.

[0068] The test select circuit starts with a three-position toggle switch 203, which drive two de-bouncers. The de-bouncer outputs are the 'PBG' and 'normal' logic steps. (See FIG. 4F) [0069] The press to test switch 204 and the G-suit switch 260 drive two de-bouncers. Their outputs are the 'TST' and "GSUIT' logic steps.

[0070] With respect to the G-suit pressure sensor 113 and the mask pressure sensor 112, the output from the G-suit pressure sensor 113 is fed into a digital indicator 268. The indicator 268 turns the input voltage into a digital signal and processes it, rescaling it into engineering units and outputting it in the form of a number presented on the indicator 268. It also provides



a TTL logic high output at 55, 70 and 138.4 in H_2O . The indicator provides 10-volt excitation for the pressure transducer. The mask transducer (sensor) 112 works the same except it outputs TTL logic high outputs at 1, 18 and 34 in H_2O . (See FIG. 4, part O)

[0071] The G-suit regulator enable valve 109 is normally closed. It is turned on to vent the G-suit regulator 108 to regulate the G-suit pressure (GSP) to 60 in H₂O, which is the normal suit operating pressure. It is turned off when performing a G-suit leak test (LK-GS).

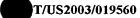
[0072] The G-suit control valve 110 is normally closed. In any mode select position other than 'LK-GS', the G-suit control valve 110 is turned on until the G-suit pressure reaches 70 in H_2O . In the 'LK-GS' position, the G-suit control valve 110 is turned on until the G-suit pressure reaches 138.4 in H_2O .

[0073] With respect to the low flow valve 105, this valve 105 is turned on until the mask pressure (MP) reaches 34 in H_2O when the press to test switch 204 is pressed in the 'LK-LO' position

[0074] The mask limit valve 114 is normally open. When the test select switch 203 is in 'normal', the mask limit valve 114 is closed when the MP (mask pressure) is less than 18 in H₂O. In the 'LK-HI' or 'LK-LO' or the test select in the 'PBG' position, the mask limit valve 114 is on until mask port pressure reaches 34 in H₂O.

[0075] The mask control valve 104 is normally closed. In the 'LK-HI' position, the mask control valve 104 is on until the mask pressure reaches 34 in H_2O . In the 'mask' position, the mask control valve 104 is on when the test select switch 203 is in the 'PBG' or 'normal' positions.

[0076] The backup mask limit valve 115 is normally open. It is closed at the same time the mask limit valve 114 is closed. Its power passes through the pressure switch 111. If the mask pressure exceeds 34 in H₂O, the pressure switch 111 opens to cut off power to the backup



mask limit valve 115. The backup mask limit valve 115 opens to reduce the mask port pressure.

[0077] The 'High-Pressure Compressor' output turns on the high-pressure compressor 103 at 55 in H_2O and off at 70 or 138.4 in H_2O . In the 'LK-GS' position, it turns off at 138.4 in H_2O .

[0078] The 'Low-Pressure Compressor 1' output turns on the low-pressure compressor 1 102a when the test select switch 203 is in either the PBG or 'normal' positions. If the mode select switch 201 is in the 'LK-HI' or 'LK-LO' position, the blower 102a is on. This is done to provide positive flow whenever the mask port is in use.

[0079] The 'Low-pressure Compressor 2' output and the 'Low-Pressure Compressor 3' output turn on the low-pressure compressor 2 as '102b' in FIG. 1 and the low-pressure compressor 3 as '102c' in FIG. 1 when the test select switch 203 is in the 'normal' or 'PBG' position and the mask pressure drops below 1 in H₂O. When the test switch 203 is in the 'normal' and the mode select switch is 'LK-LO' or 'LK-HI' position, the low-pressure compressor 2 and 3 102b and 102c are turned on when the press to test switch 204 is pushed. When the test switch 203 is in the 'PBG', the low-pressure compressor 2 and 3 102b and 102c are turned on when the press to test switch 204 is pushed and, after one minute, these two low-pressure compressors 102b and 102c are turned off.

[0080] The 'Full ON' output is used to turn on the three low-pressure compressors 102a, 102b, and 102 c of the low-pressure compressor system 102 at their maximum operating speed when they are used to inflate the G-suit. This output is high when the G-suit switch 260 is turned on if no output is required from the mask port. The 'Mask Port' output takes precedence over G-suit inflation.

[0081] If the 'Variable Speed Enable', '41 M Speed Enable', '43M Speed Enable' or '45M

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Speed Enable' is not turned on, the 'Normal Speed Enable' is on (high).

[0082] When 41M is selected, the press to test button 204 is pushed, and the test select switch 203 is in the 'normal' or 'PBG' position, the '41 M Speed Enable' is on (high).

[0083] When 43M is selected, the press to test button 204 is pushed, and the test select switch 203 is in the 'normal' or 'PBG' position, the '43M Speed Enable' is on (high).

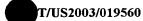
[0084] When 45M is selected, the press to test button 204 is pushed, and the test select switch 203 is in the 'normal' or 'PBG' position, the '45M Speed Enable' is on (high).

[0085] When 'LK-HI' or 'LK-LO' or 'PBG' with the press to test button 204 is pushed, the 'Variable Speed Enable' is on provided the G-suit pressure is greater than 55 in H₂O. The output from the G-suit pressure transducer (sensor) 113 is compared with a preset level to determine whether condition is being met.

[0086] The high-pressure compressor is turned on by the 'HP CMPR ON' signal. The 'HP CMPR ON' goes high when the G-suit switch is turned on and the following conditions are met; the G-suit pressure is greater than 55 in H_2O but less than 138.4 in H_2O , and the G-suit pressure is less than 70 in H_2O or 'LK-GS' mode selected.

[0087] The speed control PCB (PCB3) provides power to the three low-pressure compressors 102a, 102b and 102c. The power provided to the low-pressure compressors voltage is variable. This is done to vary the compressors output pressure. The low-pressure compressor 1 102a is turned off and on independently of the low-pressure compressors 2 102b and 3 102c. The speed control section outputs one of four fixed voltages or a variable voltage to the compressors that are turned on. Three adjustable voltage regulators tied in parallel supply the compressor voltage. Five external variable resistors set the regulators output voltage. (See FIG. 4N)

[0088] The speed control PCB (PCB3) has eight logic inputs. The logic inputs set the



variable speed control and determine which compressors are turned on. The logic inputs are 'Full On', 'the Low-Pressure Compressor 1', 'the Low-Pressure Compressor 2 and 3', 'Normal Speed Enable', '41M Speed Enable', '43M Speed Enable', '45M Speed Enable', and 'Variable Speed Enable'.

[0089] The low-pressure compressor motor outputs include four power relays. Two power relays drive the low-pressure compressor 1 motor and the other two power relays drive the low-pressure compressor 2 and 3 motors. Opto isolators drive the power relays. This is done to protect the CMOS logic from inductive spikes that occurs when switching the motors. When the 'Full On' input goes high, one set of relays turns on, outputting 15 VDC (voltage of direct current) to all three low-pressure compressor motors 102a, 102b and 102c. When either or both of the second set relays turn on, the variable voltage from the voltage regulators is outputted to the appropriate motors. (See FIG. 4M and 4N)

[0090] The pressure control 262 located on the control panel 200 is the variable resistor that is inputted to the speed control board. It is bypassed when the variable pressure switch 290 is in the 'CONST' position 290a causing the mask port pressure to stay at 16 in H20. Otherwise the output pressure can be varied between 16 and 34 in H20 when the test select switch 203 is set to 'PBG'.

[0091] As part of preflight, the user verifies his or her communication equipment. The user attaches to the tester and talks into the microphone. The sound picked up by the microphone should be clearly heard with the earphones. Audio system is made up of a preamp and a power amp. Several different kinds of microphones can be inputted into the tester. There are four different microphone inputs. The primary input is 'audio A' 222. This input is configured to accept a 5-ohm dynamic microphone when the audio select switch 236 is in the LIS/TLK 1



(listen/talk) 236b. In the LIS/TLK 2 position 236c, it is configured to interface with an Electret microphone that requires 10-VDC (voltage of direct current) bias with 8 mA (milliamperes) current limit. In this position an audio input transformer and bias circuit is added to the input circuit. The output of the audio input transformer is fed into the preamp. There are two carbon microphone inputs parallel together. The two inputs are the carbon headset jack 226 and the PTT (Press to talk) talk jack 228. These inputs 226 and 228 have 24-VDC bias current limited to 10 mA. The input from the carbon microphone is fed directly to the power amplifier bypassing the preamp. The primary audio output is through the audio A jack 222. In the LIS/TLK 1 236b, it is setup to output into a 10-ohm dynamic microphone. In the LIS/TLK 2 position 236c, it is designed to output to 600 ohm input impedance earphones. The 'audio B' jack 224 is always configured to accept 5 ohm dynamic microphone and output to a 10 ohm dynamic load. The audio A jack 222 also provides +28 VDC (voltage of direct current) up to 200 mA power. It can be used to drive an ANR (Active Noised Reduction) unit. [0092] A built in continuity tester can be provided to trouble shoot the communication gear. When the audio select switch 236 is in the 'cont' (continuity) position 236a, the communication circuits turn into a continuity tester. The carbon microphone, dynamic microphone and dynamic headset output DC resistance is monitored. If the dynamic microphone input resistance is between 4 to 7 ohms, the microphone light 230 will turn green. If it is less than 2 ohms, the microphone light 230 will turn red. If the output resistance is between 8 to 12 ohms, the earphone light 232 will turn green. If the output resistance is less than 2 ohms, the earphone light 232 will turn red. If the carbon microphone input resistance is between 80 to 500 ohms, the microphone light 230 will turn green. If it is less than 20 ohms, the microphone light will turn red. The input/output resistance of these three circuits is determined by holding the current through input/output constant. Now the resistance is



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directly proportional to the voltage. This voltage is amplified and fed into a window comparator and a limit comparator. The window comparators control the microphone/earphone green lights. If the comparators input voltage falls within the upper and lower set points, the green light will turn on. If the input voltage is less than limit comparator set voltage, the red light will turn on.

[0093] To perform a goggle test, the EEU-2P flash goggles or equivalent are attached to the tester. After 10 seconds, the PTT button 228 is pressed. The goggles will turn opaque if they are working. 28 to 32 VDC is supplied to the EEU-2P goggles through the goggle jack 238. This voltage has to be 27 VDC min (minimum voltage). when outputting 20ma into 1400 ohm. The shorted output current must be 70 mA minimum and not more than 100 mA maximum. This is accomplished with voltage regulator and current limiting circuits.

[0094] Fig. 5 illustrates a general block diagram of a portion of the present invention. The diagram includes a gas system unit 802 which includes elements such as valve and compressor units and a speed control unit (See PCB3). The gas system unit 802 is controlled by the main PCB (PCB1) which uses the logic unit 804 to control the overall operation (See FIG. 4). The logic unit 804 outputs control the speed control unit (See PCB3), and the valves that control the flow. The communication unit 806 is also included in the present invention and includes the audio unit 808 (See PCB2) which is connected to PCB1.

[0095] The present invention integrates a plurality of testers into one unit and yet requires less power than earlier systems. The unit runs on standard 115 or 230 VAC (voltage of alternating current), 47-440 Hz (hertz), 4 Amperes. Input requirements are 85-132/170-264



VAC 47-440 HZ (hertz) 400W (watts). The mask port pressure/flow output schedule is shown by the following table:

Table 1.

Setting	@ 0 LPM in H ₂ O	@ 5.0 LPM in H ₂ O
NORMAL	3.25	1.75±.5
41M	5.8	4.00±.5
43M	8.25	6.00±.5
45M	10.5	8.00±.5
PBG	16-32	NA
LK HI	16-32	NA
LK LO	16-32	NA

[0096] The tester 100 can be run from an internal rechargeable battery pack as an alternative to alternating current input from an outside source connected to for example the battery port 250. The battery pack can be nickel metal hydride batteries accessible through a weatherproof side panel. Other types of batteries such as lithium-ion and lithium-polymer can also be used. The power cord for outside power source can be attached to the back panel when the console is mounted. A built in charger can charge the tester in one hour or less or 20 minutes on the average. The tester can run up to 8 hours or more from its internal rechargeable battery pack. The duration can be increased depending on the type and size of the battery.

[0097] The G-Suit port output pressure is shown by the following table:

Table 2.

Setting	Output Press. in H ₂ O
G-suit on	58±1
G-suit leak test	0-150

[0098] An example specification of the present invention (CAST) is described as follows.

[0099] The leak indication is shown by a leak above 5.5±.5 lpm (liters per minute). The flow indication is 0-10,000±25 sccm and 0-300±1 sscm. The pressure drop leak range is 0-5 lpm. The temperature limits for the operating range is 0°C to 50°C while for storage is -40°C to 75°C. The flash goggle power is 28+2 VDC (voltage of direct current), 70-100 ma (milliamperes), current limited to 100 ma (milliamperes) maximum. The active noise reduction (ANR) power is +28±4 VDC (voltage of direct current) 200 ma (milliamperes) minimum. The microphone input current is 8 mA (milliamperes) maximum at 10 VDC (voltage of direct current).

[0100] With this configuration, the present invention can test all the aircrew's life support equipment. The present invention does not require anything more than commonly available local power to operate. The present invention is able to operate in a chemical warfare environment. The present invention does not require a separate high-pressure source of breathing air/oxygen. The present invention significantly reduces supporting man-hours, deployment costs and mobility footprint.

[0101] While the invention has been particularly shown and described with reference to the preferred embodiments thereof, it will be understood by those skilled in the art that the foregoing and other changes in form and details may be made therein without departing from the spirit and scope of the invention.

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What is claimed is:

1. A gas system for testing aircrew systems including a first system and a second system, said gas system comprising:

an input filter located in an inlet port, said input filter filtering an air to prevent foreign particles from entering said gas system

a first compressor compressing said air, said first compressor comprising at least one blower, a speed of said blower depending on a voltage applied to said blower;

a second compressor compressing said air, said second compressor producing a lower flow at a higher pressure than said first compressor;

a first flow sensor detecting a flow of the air compressed by said first compressor and a leaking of the aircrew systems;

a second flow sensor detecting the flow of the air compressed by said first compressor and the leaking of the aircrew systems;

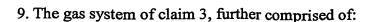
a first flow valve mounted for controlling the flow of the air compressed by said first compressor to said first flow sensor;

a second flow valve mounted for controlling the flow of the air compressed by said first compressor to said second flow sensor;

- a regulator regulating a pressure of said second system;
- a first pressure sensor detecting a pressure of said first system;
- a second pressure sensor detecting the pressure of said second system;
- a first pressure valve for controlling the pressure of said first system;
- a second pressure valve for controlling the pressure of said second system; and
- a controller controlling an operation of said gas system.

- 2. The gas system of claim 1, with said inlet filter designed to accept a chemical filter.
- 3. The gas system of claim 1, wherein said first system is a mask, and said second system is a G-suit.
- 4. The gas system of claim 3, said first compressor comprising three regenerative blowers connected in series, said three regenerative blowers comprising a first blower, a second blower, and a third blower.
- 5. The gas system of claim 4, each of said three regenerative blowers having 21 inch H₂O of a maximum output pressure.
- 6. The gas system of claim 4, said first compressor compressing the air for testing said mask, said first compressor and said second compressor in order compressing the air for testing said G-suit.
- 7. The gas system of claim 6, said first compressor compressing the air until a G-suit pressure reaches a predetermined first pressure, said second compressor starting to compress the air when said G-suit pressure reaches said predetermined first pressure and finishing when said G-suit pressure reaches a predetermined second pressure.
- 8. The gas system of claim 7, wherein said predetermined first pressure is about 55 inch H₂O, and said predetermined second pressure is about 70 inch H₂O.





said first flow sensor being able to measure the flow from 0 to 10,000 cubic centimeters per minute; and

said second flow sensor being able to measure the flow 0 to 300 cubic centimeters per minute.

- 10. The gas system of claim 3, further comprising:
- a first digital indicator reading out data outputted from said first and second flow sensors.
 - 11. The gas system of claim 10, further comprised of:

said first digital indicator converting the data to a digital signal presented as number scaled in engineering units.

- 12. The gas system of claim 10, further comprising:
- a second digital indicator reading out data outputted from said first pressure sensor; and
 - a third digital indicator reading out data outputted from said second pressure sensor.
 - 13. The gas system of claim 3, further comprising:
 - a first limit valve limiting the pressure of said first system.
 - 14. The gas system of claim 3, further comprised of said first flow valve, said second



flow valve, said first pressure valve, said second pressure valve being solenoid valves.

- 15. The gas system of claim 12, further comprised of said first limit valve being a solenoid valve.
- 16. The gas system of claim 1, with said controller comprising a main printed circuit board (PCB).
- 17. The gas system of claim 16, with said controller further comprising a speed control printed circuit board (PCB), said speed control PCB controlling said first compressor by controlling a voltage applied to said second compressor.
- 18. The gas system of claim 16, with said main PCB using CMOS (complementary metal oxide semiconductor) logic.
 - 19. An apparatus for testing aircrew systems, said apparatus comprising:
 - a first unit testing a mask;
 - a second unit testing a g-suit; and
 - a third unit testing communication systems,
 - said first unit, said second unit, and said third unit being integrated.
 - 20. The apparatus of claim 19, further comprising a fourth unit testing a goggle.
 - 21. The apparatus of claim 19, further comprised of:



said first unit and said second unit having a common gas system, said gas system comprising;

an input filter located in an inlet port, said input filter filtering an air to prevent foreign particles from entering said gas system

a first compressor compressing said air, said first compressor comprising at least one blower, a speed of said blower depending on a voltage applied to said blower;

a second compressor compressing said air, said second compressor producing a lower flow than said first compressor, said second compressor producing a higher pressure than said first compressor;

a first flow sensor detecting a flow of the compressed air and a leaking of the mask and the G-suit;

a second flow sensor detecting the flow of the compressed air and the leaking of the mask and the G-suit;

a first flow valve mounted for controlling the flow of the compressed air to said first flow sensor;

a second flow valve mounted for controlling the flow of the compressed air to said second flow sensor;

- a regulator regulating a pressure of said G-suit;
- a first pressure sensor detecting a pressure of said mask;
- a second pressure sensor detecting the pressure of said G-suit;
- a first pressure valve for controlling the pressure of said mask;
- a second pressure valve for controlling the pressure of said G-suit; and
- a controller controlling an operation of said gas system.

- 22. The apparatus of claim 21, with said inlet filter designed to accept a chemical filter.
- 23. The apparatus of claim 21, said first compressor comprising three regenerative blowers connected in series, said three regenerative blowers comprising a first blower, a second blower, and a third blower.
- 24. The apparatus of claim 21, said first compressor compressing the air for testing said mask, said first compressor compressing the air for said G-suit until a G-suit pressure reaches 55 inch H₂O, said second compressor starting to compress the air for said G-suit when said G-suit pressure is about 55 inch H₂O and finishing when said G-suit pressure is about 70 inch H₂O.
 - 25 The apparatus of claim 24, further comprised of:

said first flow sensor being able to measure the flow from 0 to 10,000 cubic centimeters per minute; and

said second flow sensor being able to measure the flow 0 to 300 cubic centimeters per minute.

- 26. The apparatus of claim 21, further comprising:
- a first digital indicator reading out data outputted from said first and second flow sensors.



- 27. The apparatus of claim 21, further comprising:
- a second digital indicator reading out data outputted from said first pressure sensor; and
 - a third digital indicator reading out data outputted from said second pressure sensor.
 - 28. The apparatus of claim 21, further comprising:
 - a first limit valve limiting a pressure of said first system.
- 29. The apparatus of claim 21, further comprised of said first flow valve, said second flow valve, said first pressure valve, said second pressure valve being solenoid valves.
- 30. The apparatus of claim 28, further comprised of said first limit valve being a solenoid valve.
 - 31. The apparatus of claim 19, further comprising a control panel.
- 32. The apparatus of claim 21, with said controller being included in a main printed circuit board.
- 33. The apparatus of claim 32, further comprising a speed control unit, said speed control unit being included in a speed control printed circuit board, said speed control unit controlling said first compressor by controlling a voltage applied to said second compressor.
 - 34. The apparatus of claim 32, with said controller including CMOS (complementary



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metal oxide semiconductor) logic.

35. The apparatus of claim 21, further comprised of:

said third unit comprising an input accommodating a microphone, an input accommodating headset, and two inputs for carbon microphones.

- 36. The apparatus of claim 35, further comprising a built-in continuity tester.
- 37. The apparatus of claim 35, with said third unit further comprising an accommodation of a second headset and microphone accommodating a first user to communicate with a second user.
- 38. A method of operating a gas system for testing aircrew systems including a first system and a second system, said method comprising the steps of:

selecting one of a test mode for a normal breathing and a test mode for a pressure breathing for Gs breathing;

filtering an ambient air with a chemical filter;

compressing said air;

detecting a flow of said air; and

detecting a pressure of said first or second system.

39. The method of claim 38, wherein said first system comprises a mask, and said second system comprises a G-suit.

- 40. The method of claim 39, wherein, when said test mode for said normal breathing is selected, the step of compressing said air further comprises the step of turning on a first compressor.
- 41. The method of claim 39, wherein, when said test mode for said pressure breathing for Gs breathing is selected, the step of compressing said air further comprises the steps of: turning on said first compressor;

turning off said first compressor and turning on said second compressor when said Gsuit pressure reaches a first predetermined point; and

turning off said second compressor when said G-suit pressure is a second predetermined point.

- 42. The method of claim 41, wherein said predetermined first pressure is about 55 inch H₂O, and said predetermined second pressure is about 70 inch H₂O.
- 43. The method of claim 41, with said first compressor comprising a first blower, a second blower, and a third blower.
- 44. The method of claim 43, with said step of compressing said air further comprising the step of:

controlling said first compressor by adjusting a voltage applied to each of said first, second, and third blowers and by deciding how many said blowers are turned on.

45. A method of testing aircrew systems including a first system and a second system



with an apparatus, said method comprising the steps of:

taking a first test for a mask at a first pressure;

putting a G-suit on a user;

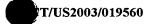
taking a second test for the mask at a second pressure with the G-suit not inflated; inflating said G-suit; and

taking a third test for the mask at a third pressure with the G-suit inflated, said second pressure being higher than said first pressure and lower than said third pressure.

- 46. The method of claim 45, wherein said first pressure is from about 1 to about 10 inch H_2O , said second pressure is about 16 inch H_2O , and said third pressure is about 32 inch H_2O .
 - 47. The method of claim 46, the second test further comprising the step of: verifying a function of said mask; and verifying that a vest starts to inflate.
- 48. The method of claim 47, further comprising the step of:

 opening a first flow valve for directing all the flow to a first flow sensor, said first flow sensor sensing 0 to approximately 10,000 cubic centimeters per minute; and checking a leak by detecting the flow with said first flow sensor.
 - 49. The method of claim 47, further comprising the step of: opening a second flow valve for directing all the flow to a second flow sensor, said

second flow sensor sensing 0 to approximately 300 cubic centimeters per minute; and



checking a leak by detecting the flow with said second flow sensor.

50. The method of claim 48, the step of taking the third test further comprising the steps of:

increasing a pressure to about 32 inch H₂O; and taking said second test at said third pressure with the G-suit inflated.

51. The method of claim 50, the step of inflating said G-suit further comprising the steps of:

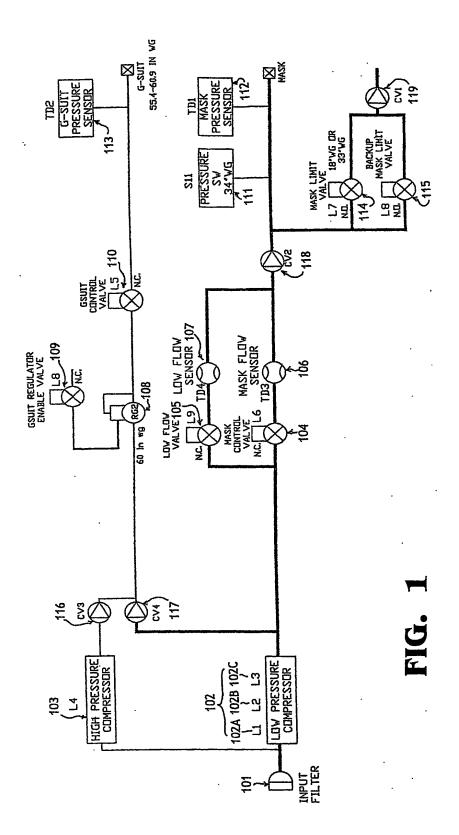
turning on said first compressor at its maximum operating speed;

turning off said first compressor and turning on said second compressor when said Gsuit pressure reaches a first predetermined point; and

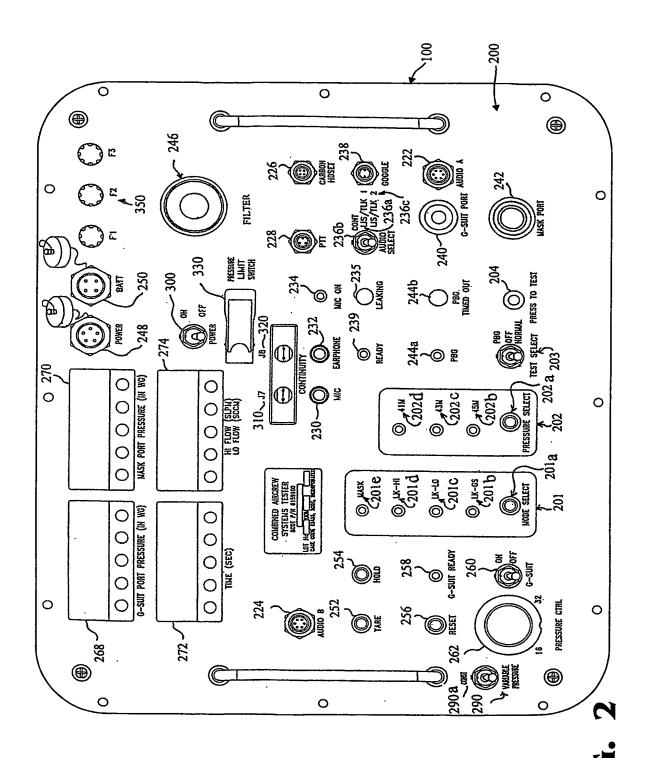
turning off said second compressor when said G-suit pressure is a second predetermined point.

- 52. The method of claim 51, wherein said predetermined first pressure is about 55 inch H₂O, and said predetermined second pressure is about 70 inch H₂O.
 - 53. The method of claim 52, further comprising the step of: increasing said pressure to about 138.4 inch H₂O; detecting a change in said pressure over an interval of time; and calculating a leak rate.



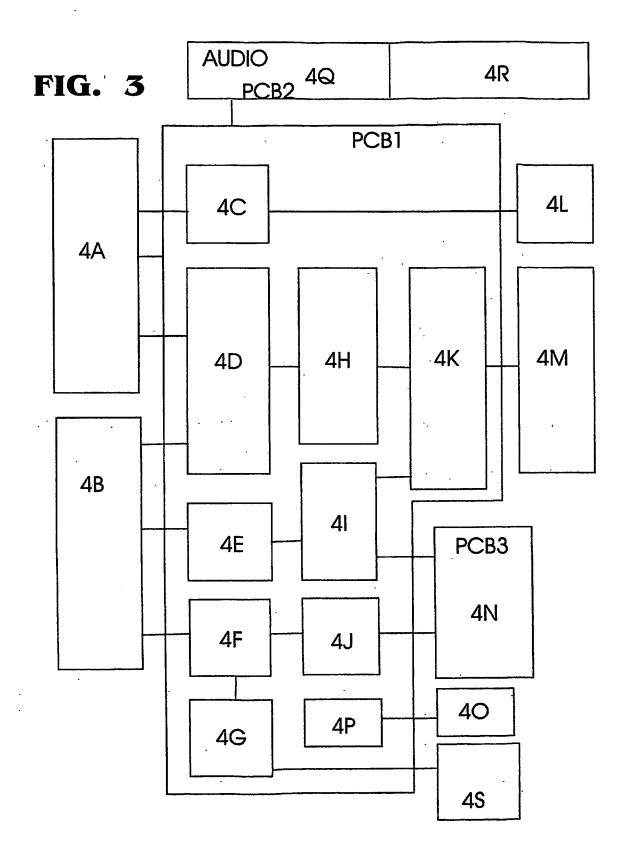


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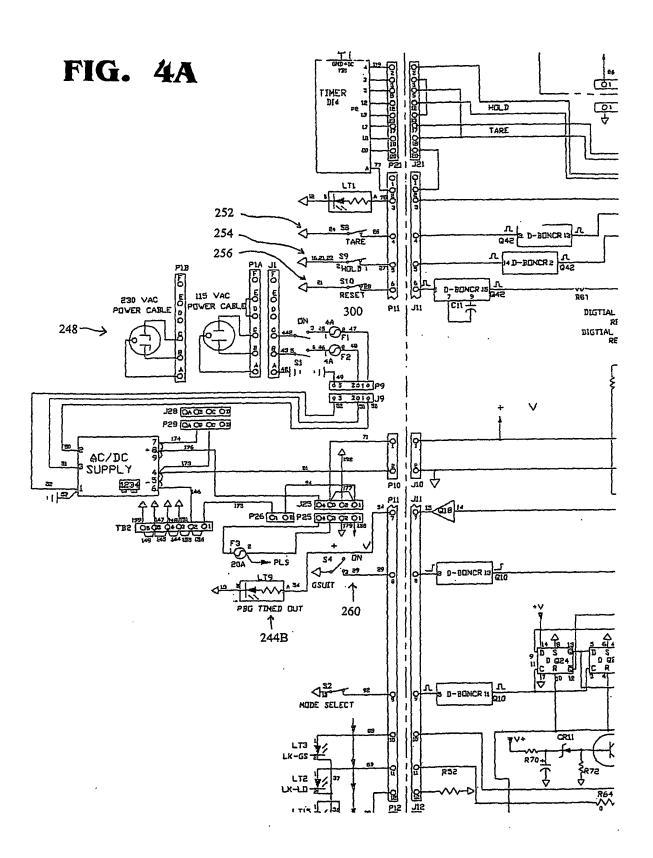


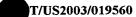
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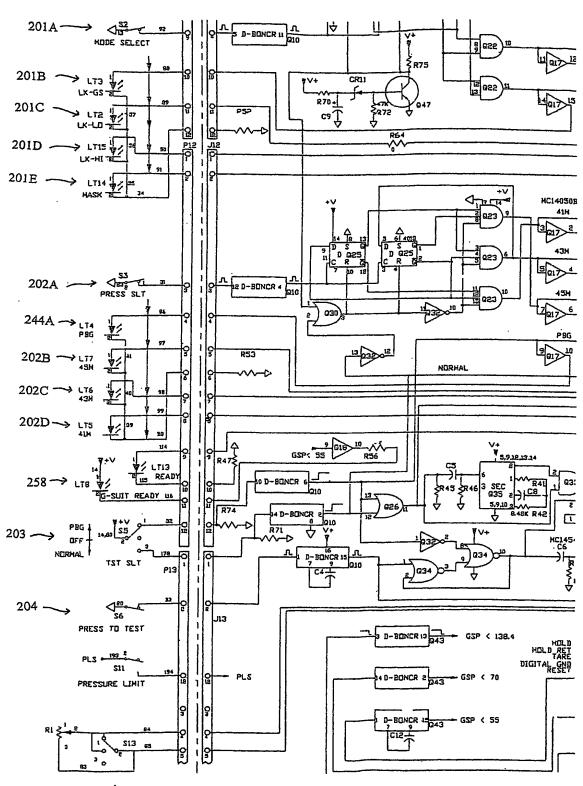
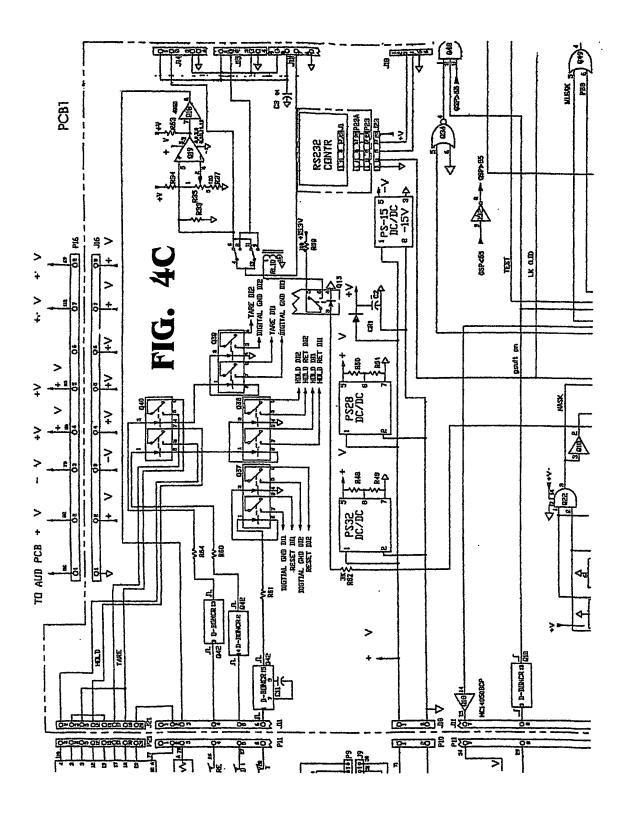
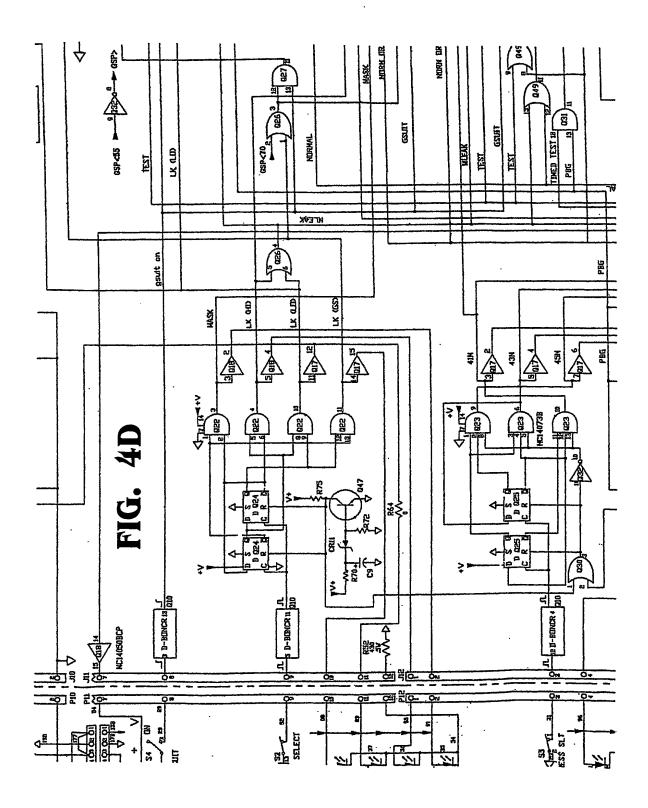


FIG. 4B

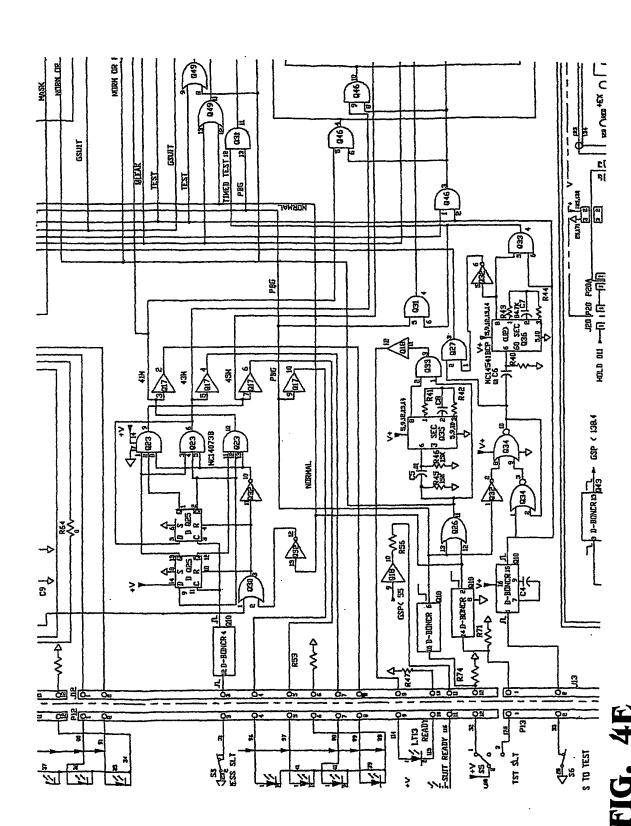






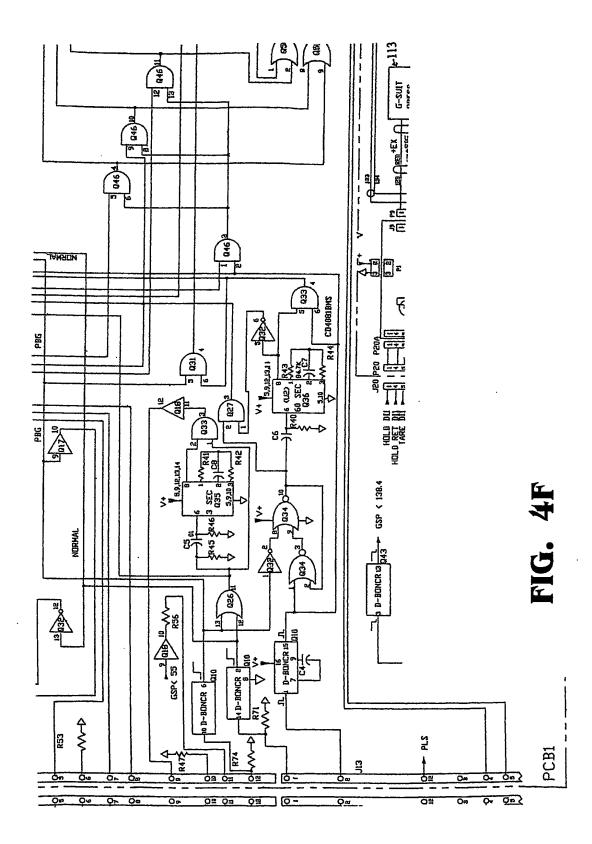


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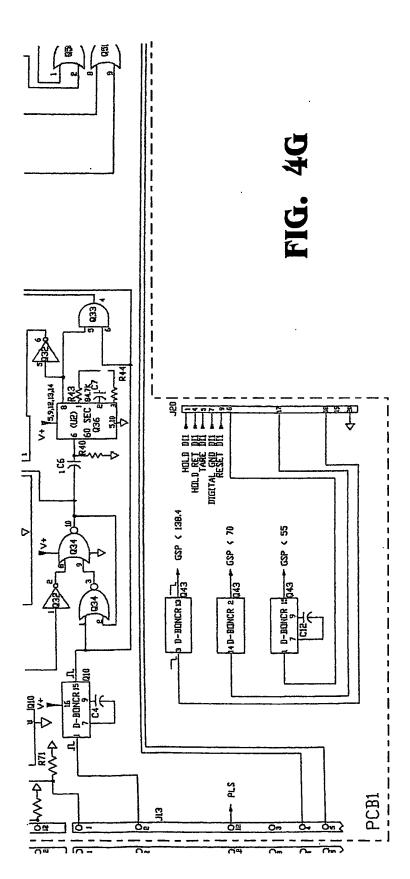


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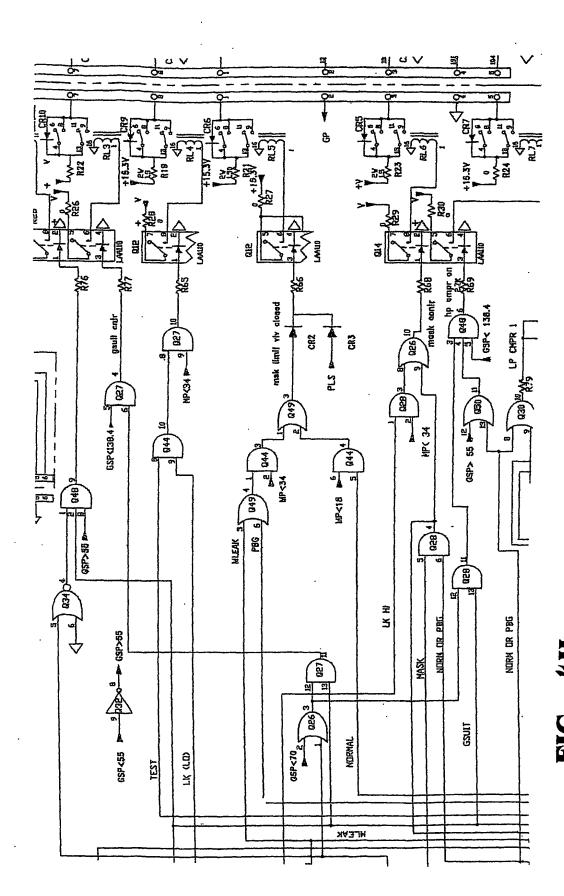












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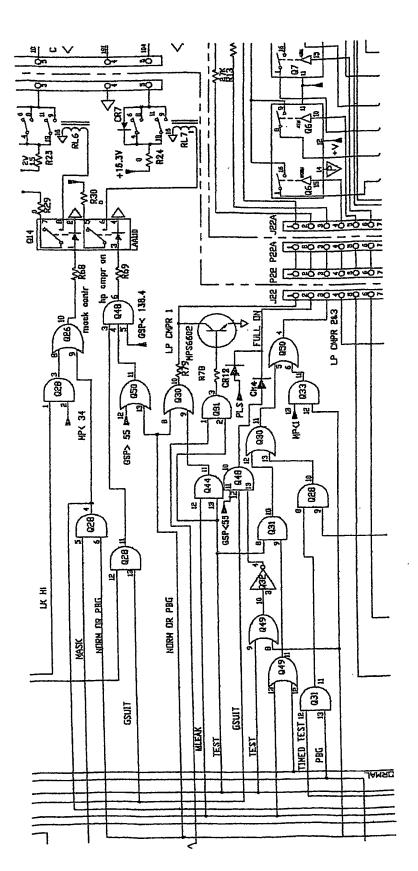
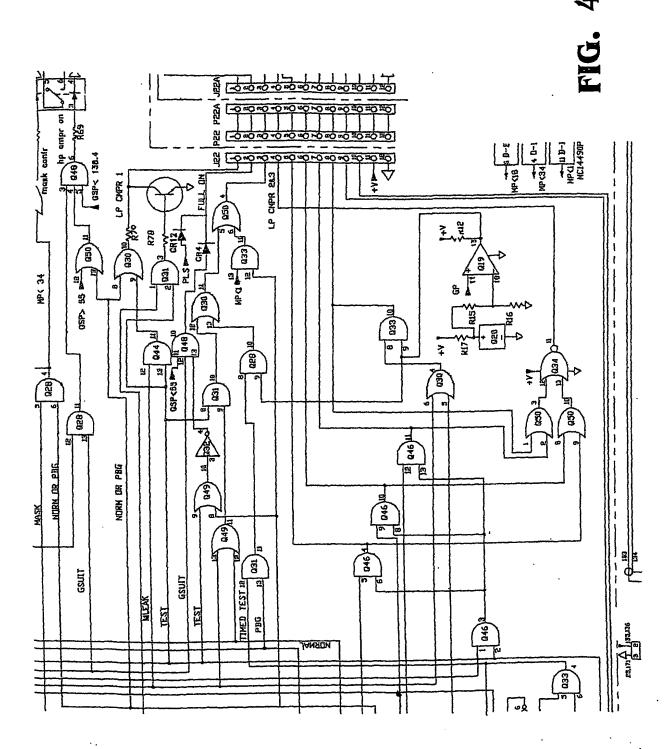


FIG. 41





0.

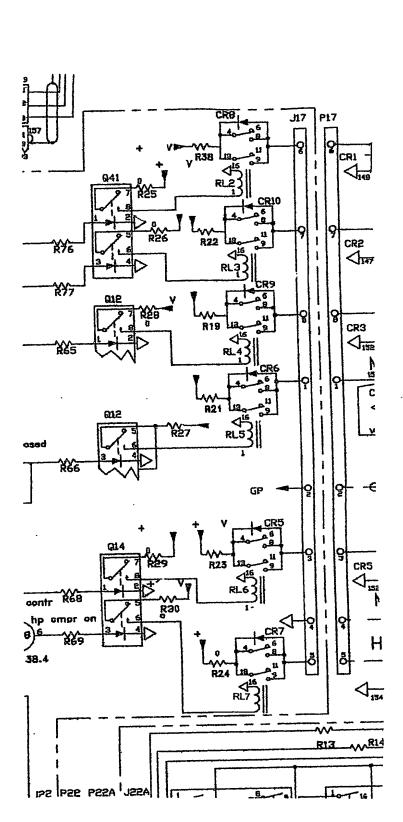
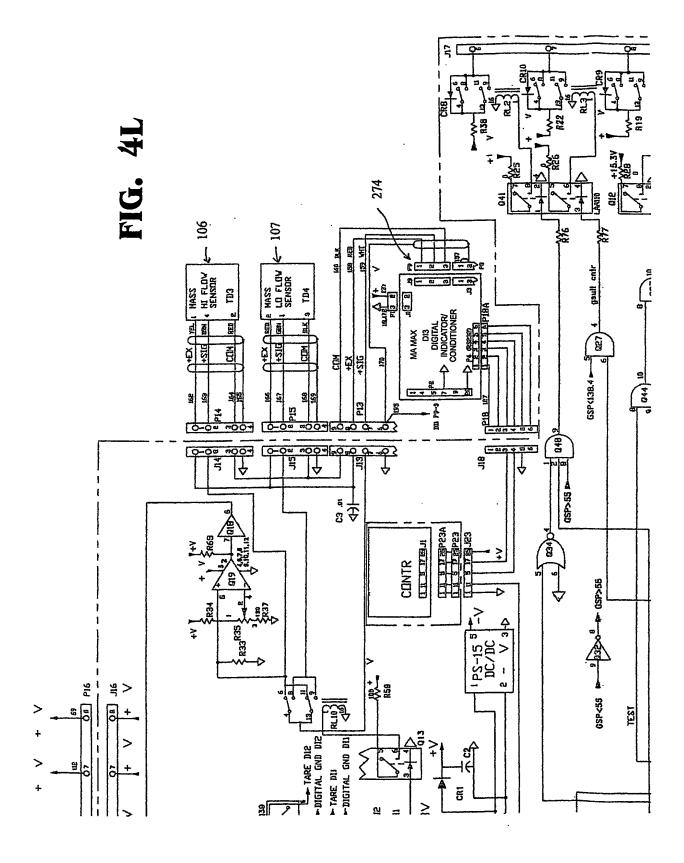
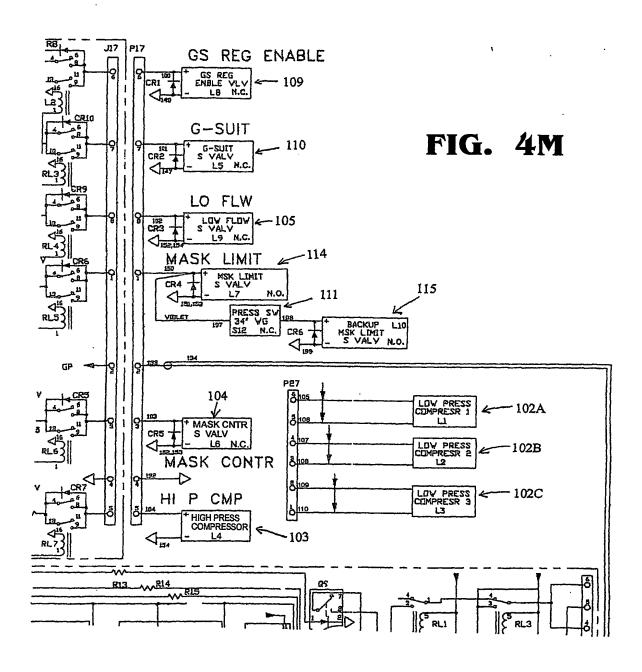


FIG. 4K







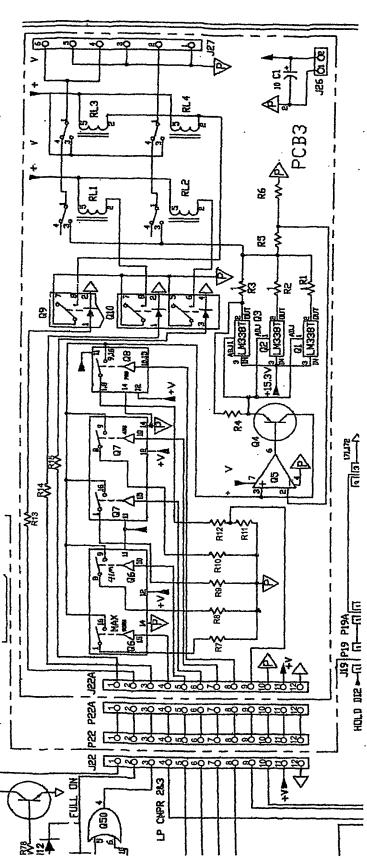


FIG. 4N



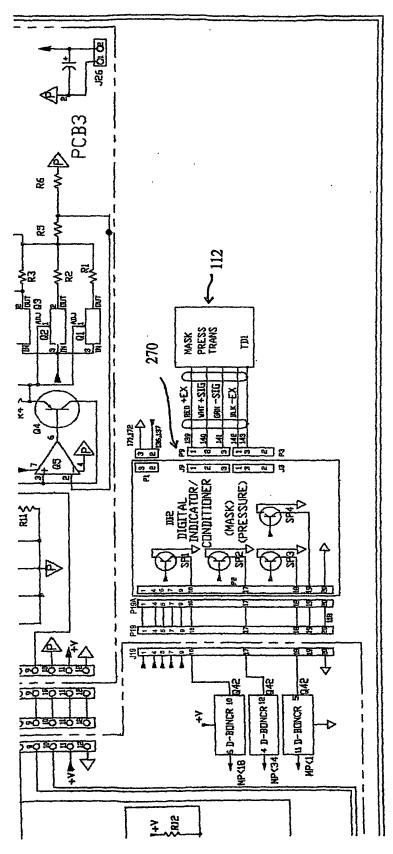
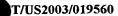


FIG. 40





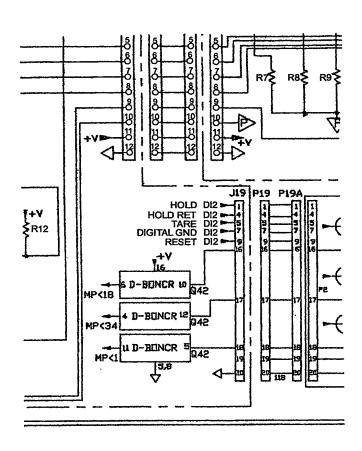
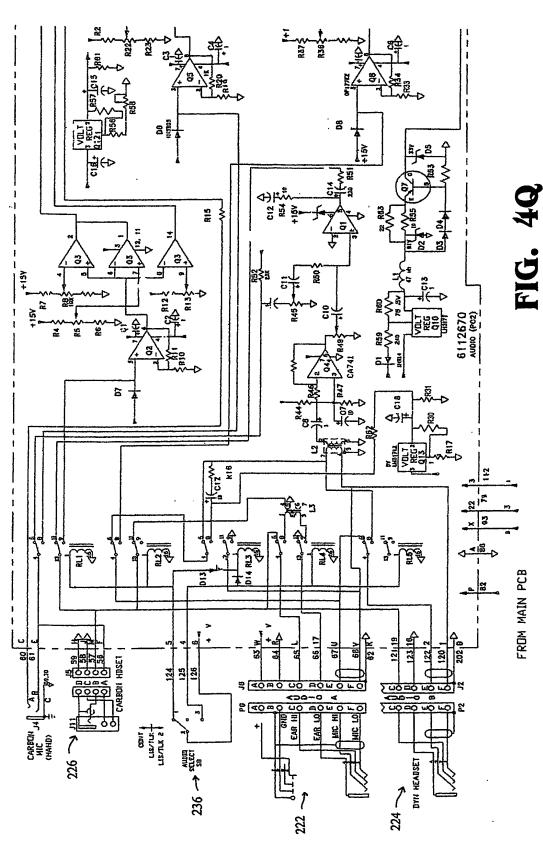


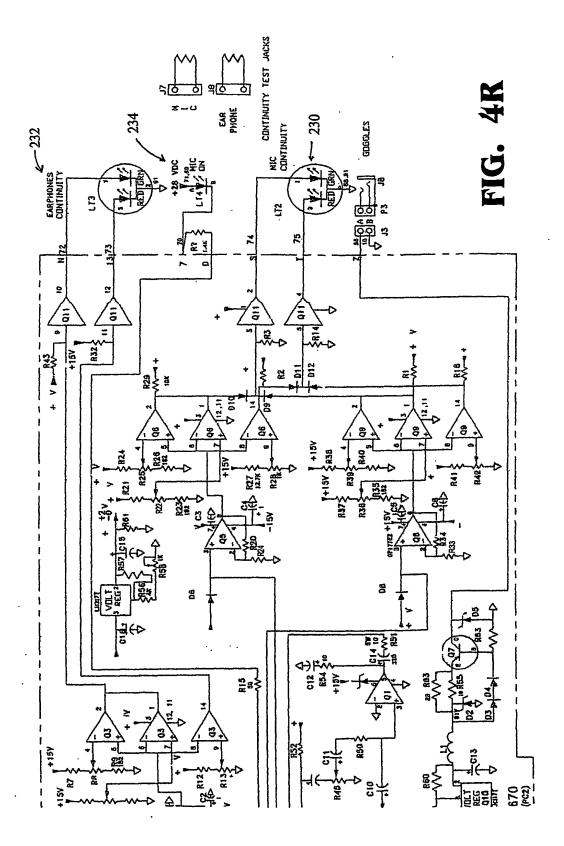
FIG. 4P

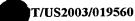


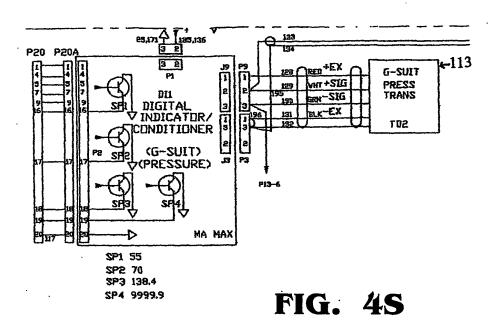


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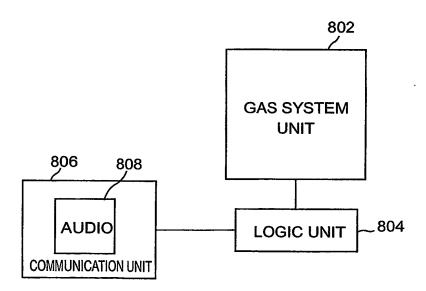


FIG. 5



INTERNATIONAL SEARCH REPORT

International application No.

		PCT/US	03/19560
A. CLASSIFICATION OF SUBJECT MATTER			
IPC(7) : A62B 17/00			
US CL: 128/202.11 According to International Patent Classification (IPC) or to both national classification and IPC			
B. FIELDS SEARCHED			
Minimum documentation searched (classification system followed by classification symbols) U.S.: Please See Continuation Sheet			
0.0 1 10200 000 001112121101			
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched			
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)			
C. DOC	UMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where a	ppropriate, of the relevant passag	ges Relevant to claim No.
X	US 5,318,018 A (PUMA et al) 7 June 1994 (07.06.1	994) column 22, lines 41-67	19, 20, 31
 Y			10. 20. 21
ı ı			19, 20, 31
Y, P	US 6,435,009 B1 (TILLEY G. A.) 20 August 2002	(20,08,2002), whole document	19, 20, 31, 38
		(11,00,01,00
A	US 6,425,395 B1 (BREWER et al) 30 July 2002 (30.07.2002), whole document		1-55
A	US 4,846,166 (WILLEKE, K.) 11 July 1989 (11.07.1989), whole document		1-55
A	US 4,344,144 (DAMICO et al) 10 August 1982 (10.08.1982), whole document		1-55
A	US 5,246,993 (MCGRADY et al) 21 September 1993 (21.09.1993), whole document		1-55
A	US 5,477,850 (ZEGLER, et al) 26 December 1995 (26.12.1995), whole document		1-55
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Further	r documents are listed in the continuation of Box C.	See patent family ann	ex
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PCT/US03/19560 INTERNATIONAL SEARCH REPORT Continuation of B. FIELDS SEARCHED Item 1: 128/202.11, 128/205.24, 128/205.25, 128/202.12, 128/202.13, 128/202.19, 128/201.19, 128/206.21, 128/206.24, 128/206.23, 454/255, 454/256, 73/40, 73/40.7, 340/605

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